Tools \&
Software

# TPS255xx Precision Adjustable Current-Limited Power-Distribution Switches 

## 1 Features

- Up to 1.5-A Maximum Load Current
- $\pm 6 \%$ Current-Limit Accuracy at 1.7 A (Typical)
- Meets USB Current-Limiting Requirements
- Backwards Compatible With TPS2550 and TPS2551
- Adjustable Current Limit: 75 mA to 1700 mA (Typical)
- Constant-Current (TPS255x) and Latch-Off (TPS255x-1) Versions
- Fast Overcurrent Response - $2 \mu \mathrm{~s}$ (Typical)
- $85-\mathrm{m} \Omega$ High-Side MOSFET (DBV Package)
- Reverse Input-Output Voltage Protection
- Operating Range: 2.5 V to 6.5 V
- Built-In Soft Start
- 15-kV ESD Protection per IEC 61000-4-2 (With External Capacitance)
- UL Listed - File No. E169910 and NEMKO IEC60950-1-am1 ed2.0
- See the TI Switch Portfolio


## 2 Applications

- USB Ports and Hubs
- Digital TVs
- Set-Top Boxes
- VOIP Phones


## 3 Description

The TPS255x and TPS255x-1 power-distribution switches are intended for applications where precision current limiting is required or heavy capacitive loads and short circuits are encountered and provide up to 1.5 A of continuous load current. These devices offer a programmable current-limit threshold between 75 mA and 1.7 A (typical) through an external resistor. Current-limit accuracy as tight as $\pm 6 \%$ can be achieved at the higher current-limit settings. The power-switch rise and fall times are controlled to minimize current surges during turnon and turnoff.
TPS255x devices limit the output current to a safe level by using a constant-current mode when the output load exceeds the current-limit threshold. TPS255x-1 devices provide circuit breaker functionality by latching off the power switch during overcurrent or reverse-voltage situations. An internal reverse-voltage comparator disables the powerswitch when the output voltage is driven higher than the input to protect devices on the input side of the switch. The FAULT output asserts low during overcurrent and reverse-voltage conditions.

Device Information ${ }^{(1)}$

| PART NUMBER | PACKAGE | BODY SIZE (NOM) |
| :--- | :--- | :--- |
| TPS2552 | SOT-23 (6) | $2.90 \mathrm{~mm} \times 1.60 \mathrm{~mm}$ |
|  | WSON (6) | $2.00 \mathrm{~mm} \times 2.00 \mathrm{~mm}$ |
| TPS2553 | SOT-23 (6) | $2.90 \mathrm{~mm} \times 1.60 \mathrm{~mm}$ |
|  | WSON (6) | $2.00 \mathrm{~mm} \times 2.00 \mathrm{~mm}$ |

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Typical Application


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## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.
Changes from Revision E (February 2012) to Revision F Page

- Added ESD Rating table, Feature Description section, Device Functional Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device and Documentation Support section, and Mechanical, Packaging, and Orderable Information section ..... 1
- Changed 1300 mA to 1700 mA in the adjustable current limit bullet under the Features section ..... 1
- Changed from 1.2 A to 1.5 A. ..... 4
Changes from Revision D (June 2011) to Revision E ..... Page
- Changed $\mathrm{V}_{\mathrm{EN}}$ to $\mathrm{V}_{\overline{\mathrm{EN}}}$ in Recommended Operating Conditions ..... 6
- Changed $\mathrm{V}_{\overline{\mathrm{EN}}}$ to $\mathrm{V}_{\mathrm{EN}}$ in Recommended Operating Conditions ..... 6
Changes from Revision C (September 2009) to Revision D Page
- Changed From: Fast Overcurrent Response - $2-\mu \mathrm{S}$ (typ) To: Fast Overcurrent Response - $2-\mu \mathrm{s}$ (typ) in the Features ..... 1
- Added text To Feature - UL Listed "and NEMKO IEC60950-1-am1 ed2.0" ..... 1
- Added Features Item "See the TI Switch Portfoilo" ..... 1
- Changed the DEVICE INFORMATION table, and Deleted Note 3 ..... 1
- Added ESD-system level (contact/air) to the ABS MAX table, and Added Note 3 ..... 6
- Added text to the REVERSE-VOLTAGE PROTECTION section: "A reverse.....when this occurs." ..... 14
Changes from Revision B (February 2009) to Revision C ..... Page
- Added Feature - Up to 1.5 A Maximum Load Current ..... 1
- Changed 1.3 A (typ) To: 1.7 A (typ) ..... 1
- Added Text - and provide up to 1.5 A of continuous load current ..... 1
- Changed From: $19.1 \mathrm{k} \Omega \leq \mathrm{R}_{\text {LIM }} \leq 232 \mathrm{k} \Omega$ To: $15 \mathrm{k} \Omega \leq \mathrm{R}_{\text {LIM }} \leq 232 \mathrm{k} \Omega$. ..... 5
- Changed $\mathrm{l}_{\text {out }}$ values for 1.2 A and 1.5 A ..... 6
- Changed $\mathrm{T}_{\mathrm{J}}$ values for 1.2A and 1.5A ..... 6
- Added $\mathrm{R}_{\mathrm{LLI}}=15 \mathrm{k} \Omega$ option ..... 7
- Changed Text From: current-limit threshold between 75 mA and 1.3 A (typ) To: current-limit threshold between 75 mA and 1.7 A (typ) ..... 13
- Changed Text From: The recommended $1 \%$ resistor range for $R_{\text {ILIM }}$ is $19.1 \mathrm{k} \Omega \leq R_{\text {ILIM }} \leq 232 \mathrm{k} \Omega$ to ensure stability To: The recommended $1 \%$ resistor range for $R_{\text {ILIM }}$ is $15 \mathrm{k} \Omega \leq R_{\text {ILIM }} \leq 232 \mathrm{k} \Omega$ to ensure stability ..... 15
- Changed From: where $19.1 \mathrm{k} \Omega \leq \mathrm{R}_{\text {IIM }} \leq 232 \mathrm{k} \Omega$. To: where $15 \mathrm{k} \Omega \leq \mathrm{R}_{\text {ILIM }} \leq 232 \mathrm{k} \Omega$ ..... 15
- Changed Figure 23 - Current-Limit Threshold vs $\mathrm{R}_{\text {LIM }}$ ..... 16
- Changed Table 2 - added rows for Current Limit of 1400 to 1700 ..... 19
Changes from Revision A (December 2008) to Revision B Page
- Added To Features - UL Listed - File No. E169910 ..... 1
- Changed Figure 17 Ttitle From: Current Limit Threshold Vs $\mathrm{R}_{\mathrm{LLM}}$ ..... 9
- Changed Figure 18 Ttitle From: Current Limit Threshold Vs R ILM ..... 9
Changes from Original (November 2008) to Revision A Page
- Changed Title from: Adjustable Current-Limited Power-Distribution Switches to: Precision Adjustable Current- Limited Power-Distribution Switches ..... 1


## 5 Device Comparison Table

| GENERAL SWITCH CATALOG |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $33 \mathrm{~m} \Omega$, single TPS201xA 0.2A-2A TPS202x TPS203x $0.2 \mathrm{~A}-2 \mathrm{~A}-2 \mathrm{~A}$ | $80 \mathrm{~m} \Omega$, single  <br> TPS2014 600 mA <br> TPS2015 1 A <br> TPS20418 500 mA <br> TPS2051 500 mA <br> TPS2045A 250 mA <br> TPS2049 100 mA <br> TPS2055A 250 mA <br> TPS2061 1 A <br> TPS2065 1 A <br> TPS2068 1.5 A <br> TPS2069 1.5 A | $80 \mathrm{~m} \Omega$, dual  <br> TPS2042B 500 mA <br> TPS2052B 500 mA <br> TPS2046B 250 mA <br> TPS2056 250 mA <br> TPS2062 1 A <br> TPS2066 1 A <br> TPS2060 1.5 A <br> TPS2064 1.5 A |  | $80 \mathrm{~m} \Omega$, triple <br> TPS2043B 500 mA TPS2053B 500 mA TPS2047B 250 mA TPS2057A 250 mA TPS2063 1A TPS2067 1A | $80 \mathrm{~m} \Omega$, quad <br> TPS2044B 500 mA TPS2054B 500 mA TPS2048A 250 mA TPS2058 250 mA | $80 \mathrm{~m} \Omega$, quad |

## 6 Pin Configuration and Functions


$\mathrm{EN}=$ Active Low for the TPS2552
EN = Active High for the TPS2553
Add -1 to part number for latch-off version

| TPS255x DRV Package 6-Pin WSON Top View |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { UT } \\ & \text { IM } \end{aligned}$ | 2 | PAD | 6 | GN |
| FAULT | 3 |  |  | E |

EN = Active Low for the TPS2552
EN = Active High for the TPS2553
Add -1 to part number for latch-off version

Pin Functions

| PIN |  |  |  |  | 1/0 | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NAME | TPS2552 |  | TPS2553 |  |  |  |
|  | SOT-23 | WSON | SOT-23 | WSON |  |  |
| $\overline{\mathrm{EN}}$ | 3 | 4 | - | - | I | Enable input, logic low turns on power switch |
| EN | - | - | 3 | 4 | 1 | Enable input, logic high turns on power switch |
| FAULT | 4 | 3 | 4 | 3 | O | Active-low open-drain output, asserted during overcurrent, overtemperature, or reverse-voltage conditions. |
| GND | 2 | 5 | 2 | 5 | - | Ground connection; connect externally to PowerPAD |
| ILIM | 5 | 2 | 5 | 2 | O | External resistor used to set current-limit threshold; recommended $15 \mathrm{k} \Omega \leq \mathrm{R}_{\mathrm{ILIM}} \leq 232 \mathrm{k} \Omega$. |
| IN | 1 | 6 | 1 | 6 | 1 | Input voltage; connect a $0.1 \mu \mathrm{~F}$ or greater ceramic capacitor from IN to GND as close to the IC as possible. |
| OUT | 6 | 1 | 6 | 1 | O | Power-switch output |
| PowerPAD ${ }^{\text {TM }}$ | - | PAD | - | PAD | - | Internally connected to GND; used to heat-sink the part to the circuit board traces. Connect PowerPAD to GND pin externally. |

## Add -1 for Latch-Off version

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) ${ }^{(1)(2)}$

|  | MIN MAX | UNIT |
| :---: | :---: | :---: |
| Voltage range on IN, OUT, EN or $\overline{\text { EN, ILIM, }} \overline{\text { FAULT }}$ | -0.3 7 | V |
| Voltage range from IN to OUT | -7 7 | V |
| Io Continuous output current | Internally Limited |  |
| Continuous total power dissipation | See the Thermal Information |  |
| Continuous FAULT sink current | 025 | mA |
| ILIM source current | $0 \quad 1$ | mA |
| $\mathrm{T}_{\mathrm{J}} \quad$ Maximum junction temperature | -40 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {stg }}$ Storage temperature | -65 150 | ${ }^{\circ} \mathrm{C}$ |

[^0]
### 7.2 ESD Ratings

|  |  |  | VALUE | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| $V_{\text {(ESD) }}$ | Electrostatic discharge | Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 ${ }^{(1)}$ | $\pm 2000$ | V |
|  |  | Charged device model (CDM), per JEDEC specification JESD22C101 ${ }^{\text {(2) }}$ | $\pm 500$ |  |
|  |  | IEC 61000-4-2 contact discharge ${ }^{(3)}$ | $\pm 8000$ |  |
|  |  | IEC 61000-4-2 air-gap discharge ${ }^{(3)}$ | $\pm 15000$ |  |

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.
(3) Surges per EN61000-4-2. 1999 applied to output terminals of EVM. These are passing test levels, not failure threshold.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

|  |  |  | MIN | NOM MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | Input voltage, IN |  | 2.5 | 6.5 | V |
| $V_{\text {EN }}$ | Enable voltage | TPS2552/52-1 | 0 | 6.5 | V |
| $\mathrm{V}_{\text {EN }}$ | Enable voltage | TPS2553/53-1 | 0 | 6.5 | V |
| $\mathrm{V}_{\mathrm{IH}}$ | High-level input voltage on EN or EN |  | 1.1 |  | V |
| $\mathrm{V}_{\mathrm{IL}}$ | Low-level input voltage on EN or EN |  |  | 0.66 | V |
| lout | Continuous output current, OUT | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{J} \leq 125^{\circ} \mathrm{C}$ | 0 | 1.2 | A |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{J}} \leq 105^{\circ} \mathrm{C}$ | 0 | 1.5 |  |
| $\mathrm{R}_{\text {ILIM }}$ | Current-limit threshold resistor range (nominal 1\%) from ILIM to GND |  | 15 | 232 | $\mathrm{k} \Omega$ |
| $\mathrm{l}_{0}$ | Continuous FAULT sink current |  | 0 | 10 | mA |
|  | Input de-coupling capacitance, IN to GND |  | 0.1 |  | $\mu \mathrm{F}$ |
| $\mathrm{T}_{J}$ | Operating virtual junction temperature ${ }^{(1)}$ | $\mathrm{l}_{\text {OUT }} \leq 1.2 \mathrm{~A}$ | -40 | 125 | ${ }^{\circ} \mathrm{C}$ |
|  |  | $\mathrm{l}_{\text {OUT }} \leq 1.5 \mathrm{~A}$ | -40 | 105 |  |

(1) See Power Dissipation and Junction Temperature for details on how to calculate maximum junction temperature for specific applications and packages.

### 7.4 Thermal Information

| THERMAL METRIC ${ }^{(1)}$ | TPS2552 |  | TPS2553 |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | DBV (SOT-23) | DRV (WSON) | DBV (SOT-23) | DRV (WSON) |  |
|  | 6 PINS | 6 PINS | 6 PINS | 6 PINS |  |
| $\mathrm{R}_{\text {өJA }}$ Junction-to-ambient thermal resistance | 182.6 | 72 | 182.6 | 72 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $R_{\theta \text { OCC(to }}$ p) | 122.2 | 85.3 | 122.2 | 85.3 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {өJB }}$ Junction-to-board thermal resistance | 29.4 | 41.3 | 29.4 | 41.3 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| \%JT Junction-to-top characterization parameter | 20.8 | 1.7 | 20.8 | 1.7 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\psi_{\text {JB }}$ Junction-to-board characterization parameter | 28.9 | 41.7 | 28.9 | 41.7 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| R $\begin{array}{l}\text { eJC(b } \\ \text { ot) }\end{array}$ Junction-to-case (bottom) thermal resistance | - | 11.1 | - | 11.1 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

[^1]
### 7.5 Electrical Characteristics

over recommended operating conditions, $\mathrm{V}_{\overline{\mathrm{EN}}}=0 \mathrm{~V}$, or $\mathrm{V}_{\mathrm{EN}}=\mathrm{V}_{\mathrm{IN}}, \mathrm{R}_{\mathrm{FAULT}}=10 \mathrm{k} \Omega$ (unless otherwise noted)

(1) Pulse-testing techniques maintain junction temperature close to ambient temperature; thermal effects must be taken into account separately.

### 7.6 Typical Characteristics



Figure 1. Turnon Delay and Rise Time


Figure 3. Device Enabled into Short-Circuit


Figure 5. Short-Circuit to Full-Load Recovery Response


Figure 2. Turnoff Delay and Fall Time


Figure 4. Full-Load to Short-Circuit Transient Response


Figure 6. No-Load to Short-Circuit Transient Response

## Typical Characteristics (continued)



Figure 7. Short-Circuit to No-Load Recovery Response


Figure 9. 1- $\Omega$ to No Load Transient Response


Figure 11. Reverse-Voltage Protection Recovery


Figure 8. No Load to $1-\Omega$ Transient Response


Figure 10. Reverse-Voltage Protection Response


Figure 12. UVLO - Undervoltage Lockout - V

## Typical Characteristics (continued)



Figure 13. $\mathrm{I}_{\mathrm{N}}$ - Supply Current, Output Disabled - $\mu \mathrm{A}$


Figure 15. Current Limit Response - $\mu \mathrm{s}$


Figure 17. Switch Current Vs. Drain-Source Voltage Across Switch


Figure 14. $\mathrm{I}_{\mathrm{IN}}$ - Supply Current, Output Enabled - $\mu \mathrm{A}$


Figure 16. MOSFET $r_{\text {DS(on) }}$ Vs. Junction Temperature


Figure 18. Switch Current Vs. Drain-Source Voltage Across Switch

## 8 Parameter Measurement Information



Figure 19. Typical Characteristics Reference Schematic


Figure 20. Test Circuit and Voltage Waveforms


Figure 21. Response Time to Short-Circuit Waveform

## Parameter Measurement Information (continued)



Figure 22. Output Voltage vs Current-Limit Threshold

## 9 Detailed Description

### 9.1 Overview

The TPS255x and TPS255x-1 are current-limited, power-distribution switches using N-channel MOSFETs for applications where short circuits or heavy capacitive loads are encountered and provide up to 1.5 A of continuous load current. These devices allow the user to program the current-limit threshold between 75 mA and 1.7 A (typical) through an external resistor. Additional device shutdown features include overtemperature protection and reverse-voltage protection. The device incorporates an internal charge pump and gate drive circuitry necessary to drive the N-channel MOSFET. The charge pump supplies power to the driver circuit and provides the necessary voltage to pull the gate of the MOSFET above the source. The charge pump operates from input voltages as low as 2.5 V and requires little supply current. The driver controls the gate voltage of the power switch. The driver incorporates circuitry that controls the rise and fall times of the output voltage to limit large current and voltage surges and provides built-in soft-start functionality. There are two device families that handle overcurrent situations differently. The TPS255x family enters constant-current mode while the TPS255x-1 family latches off when the load exceeds the current-limit threshold.

### 9.2 Functional Block Diagram



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A. TPS255x parts enter constant current mode during current limit condition; TPS255x-1 parts latch off

### 9.3 Feature Description

### 9.3.1 Overcurrent Conditions

The TPS255x and TPS255x-1 respond to overcurrent conditions by limiting their output current to the los levels shown in Figure 23. When an overcurrent condition is detected, the device maintains a constant output current and reduces the output voltage accordingly. Two possible overload conditions can occur.

The first condition is when a short circuit or partial short circuit is present when the device is powered-up or enabled. The output voltage is held near zero potential with respect to ground and the TPS255x ramps the output current to los. The TPS255x devices limits the current to Ios until the overload condition is removed or the device begins to thermal cycle. The TPS255x-1 devices will limit the current to $I_{\text {Os }}$ until the overload condition is removed or the internal deglitch time ( $7.5-\mathrm{ms}$ typical) is reached and the device is turned off. The device remains off until power is cycled or the device enable is toggled.

## Feature Description (continued)

The second condition is when a short circuit, partial short circuit, or transient overload occurs while the device is enabled and powered on. The device responds to the overcurrent condition within time tios (see Figure 21). The current-sense amplifier is overdriven during this time and momentarily disables the internal current-limit MOSFET. The current-sense amplifier recovers and limits the output current to $\mathrm{I}_{\text {Os }}$. Similar to the previous case, the TPS255x limits the current to Ios until the overload condition is removed or the device begins to thermal cycle; the TPS255x-1 limits the current to $\mathrm{I}_{\text {os }}$ until the overload condition is removed or the internal deglitch time is reached and the device is latched off.
The TPS255x thermal cycles if an overload condition is present long enough to activate thermal limiting in any of the above cases. The device turns off when the junction temperature exceeds $135^{\circ} \mathrm{C}$ (typical) while in current limit. The device remains off until the junction temperature cools $10^{\circ} \mathrm{C}$ (typical) and then restarts. The TPS255x cycles on and off until the overload is removed (see Figure 5 and Figure 7).

### 9.3.2 Reverse-Voltage Protection

The reverse-voltage protection feature turns off the N-channel MOSFET whenever the output voltage exceeds the input voltage by 135 mV (typical) for $4-\mathrm{ms}$ (typical). A reverse current of ( $\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }} / r_{\mathrm{DS}}$ (on) $)$ are present when this occurs. This prevents damage to devices on the input side of the TPS255x and TPS2552-1/TPS2253-1 by preventing significant current from sinking into the input capacitance. The TPS255x devices allow the N-channel MOSFET to turn on once the output voltage goes below the input voltage for the same 4 -ms deglitch time. The TPS255x-1 devices keep the device turned off even if the reverse-voltage condition is removed and do not allow the N-channel MOSFET to turn on until power is cycled or the device enable is toggled. The reverse-voltage comparator also asserts the FAULT output (active-low) after 4-ms.

### 9.3.3 FAULT Response

The $\overline{\text { FAULT }}$ open-drain output is asserted (active low) during an overcurrent, overtemperature, or reverse-voltage condition. The TPS255x asserts the FAULT signal until the fault condition is removed and the device resumes normal operation. The TPS255x-1 asserts the FAULT signal during a fault condition and remains asserted while the part is latched-off. The FAULT signal is de-asserted once device power is cycled or the enable is toggled and the device resumes normal operation. The TPS255x and TPS255x-1 are designed to eliminate false FAULT reporting by using an internal delay de-glitch circuit for overcurrent ( $7.5-\mathrm{ms}$ typical) and reverse-voltage (4-ms typical) conditions without the need for external circuitry. This ensures that FAULT is not accidentally asserted due to normal operation such as starting into a heavy capacitive load. The deglitch circuitry delays entering and leaving fault conditions. Overtemperature conditions are not deglitched and assert the FAULT signal immediately.

### 9.3.4 Undervoltage Lockout (UVLO)

The undervoltage lockout (UVLO) circuit disables the power switch until the input voltage reaches the UVLO turnon threshold. Built-in hysteresis prevents unwanted on and off cycling due to input voltage drop from large current surges.

### 9.3.5 ENABLE ( $\overline{\mathrm{EN}}$ or EN)

The logic enable controls the power switch, bias for the charge pump, driver, and other circuits to reduce the supply current. The supply current is reduced to less than $1-\mu \mathrm{A}$ when a logic low is present on EN. A logic low input on EN or a logic high input on EN enables the driver, control circuits, and power switch. The enable input is compatible with both TTL and CMOS logic levels.

### 9.3.6 Thermal Sense

The TPS255x and TPS255x-1 have self-protection features using two independent thermal-sensing circuits that monitor the operating temperature of the power switch and disable operation if the temperature exceeds recommended operating conditions. The TPS255x device operates in constant-current mode during an overcurrent conditions, which increases the voltage drop across power-switch. The power dissipation in the package is proportional to the voltage drop across the power switch, which increases the junction temperature during an overcurrent condition. The first thermal sensor turns off the power switch when the die temperature exceeds $135^{\circ} \mathrm{C}$ (minimum) and the part is in current limit. Hysteresis is built into the thermal sensor, and the switch turns on after the device has cooled approximately $10^{\circ} \mathrm{C}$.

## Feature Description (continued)

The TPS255x and TPS255x-1 also have a second ambient thermal sensor. The ambient thermal sensor turns off the power-switch when the die temperature exceeds $155^{\circ} \mathrm{C}$ (minimum) regardless of whether the power switch is in current limit and turns on the power switch after the device has cooled approximately $10^{\circ} \mathrm{C}$. The TPS255x and TPS255x-1 families continue to cycle off and on until the fault is removed.
The open-drain fault reporting output FAULT is asserted (active low) immediately during an overtemperature shutdown condition.

### 9.4 Device Functional Modes

There are no other functional modes.

### 9.5 Programming

### 9.5.1 Programming the Current-Limit Threshold

The overcurrent threshold is user programmable through an external resistor. The TPS255x and TPS255x-1 use an internal regulation loop to provide a regulated voltage on the ILIM pin. The current-limit threshold is proportional to the current sourced out of ILIM. The recommended $1 \%$ resistor range for $R_{\text {ILIM }}$ is $15 \mathrm{k} \Omega \leq R_{\text {ILIM }} \leq$ $232 \mathrm{k} \Omega$ to ensure stability of the internal regulation loop. Many applications require that the minimum current limit is above a certain current level or that the maximum current limit is below a certain current level, so it is important to consider the tolerance of the overcurrent threshold when selecting a value for $\mathrm{R}_{\text {IIIM }}$. The following equations and Figure 23 can be used to calculate the resulting overcurrent threshold for a given external resistor value ( $\mathrm{R}_{\text {IIIM }}$ ). Figure 23 includes current-limit tolerance due to variations caused by temperature and process. However, the equations do not account for tolerance due to external resistor variation, so it is important to account for this tolerance when selecting $\mathrm{R}_{\mathrm{IIIM}}$. The traces routing the $\mathrm{R}_{\mathrm{ILIM}}$ resistor to the TPS255x and TPS255x-1 must be as short as possible to reduce parasitic effects on the current-limit accuracy.
$\mathrm{R}_{\text {LIIM }}$ can be selected to provide a current-limit threshold that occurs 1) above a minimum load current or 2 ) below a maximum load current.
To design above a minimum current-limit threshold, find the intersection of $\mathrm{R}_{\mathrm{ILI}}$ and the maximum desired load current on the $\mathrm{I}_{\mathrm{OS}(\text { min) }}$ curve and choose a value of $\mathrm{R}_{\text {ILIM }}$ below this value. Programming the current limit above a minimum threshold is important to ensure start-up into full load or heavy capacitive loads. The resulting maximum current-limit threshold is the intersection of the selected value of $\mathrm{R}_{\mathrm{ILIM}}$ and the $\mathrm{I}_{\mathrm{OS}(\operatorname{max)}}$ curve.
To design below a maximum current-limit threshold, find the intersection of $\mathrm{R}_{\text {LIM }}$ and the maximum desired load current on the $\mathrm{I}_{\mathrm{OS} \text { (max) }}$ curve and choose a value of $\mathrm{R}_{\mathrm{LIIM}}$ above this value. Programming the current limit below a maximum threshold is important to avoid current limiting upstream power supplies, causing the input voltage bus to droop. The resulting minimum current-limit threshold is the intersection of the selected value of $\mathrm{R}_{\text {IIIM }}$ and the $\mathrm{l}_{\mathrm{OS}(\text { min })}$ curve.
Current-Limit Threshold Equations (los):

$$
\begin{aligned}
& \mathrm{I}_{\text {OSmax }}(\mathrm{mA})=\frac{22980 \mathrm{~V}}{\mathrm{R}_{\text {LIM }}^{0.94} \mathrm{k} \Omega} \\
& \mathrm{I}_{\mathrm{OSnom}}(\mathrm{~mA})=\frac{23950 \mathrm{~V}}{\mathrm{R}_{\text {RIM }} \mathrm{ma}^{9.97} \mathrm{k} \Omega} \\
& \mathrm{l}_{\mathrm{OSmin}}(\mathrm{~mA})=\frac{25230 \mathrm{~V}}{\mathrm{R}_{\text {LIM }}{ }^{1.016} \mathrm{k} \Omega}
\end{aligned}
$$

where
$15 \mathrm{k} \Omega \leq \mathrm{R}_{\text {IIIM }} \leq 232 \mathrm{k} \Omega$.
While the maximum recommended value of RILIM is $232 \mathrm{k} \Omega$, there is one additional configuration that allows for a lower current-limit threshold. The ILIM pin may be connected directly to IN to provide a 75 mA (typical) currentlimit threshold. Additional low-ESR ceramic capacitance may be necessary from IN to GND in this configuration to prevent unwanted noise from coupling into the sensitive ILIM circuitry.

## Programming (continued)



Figure 23. Current-Limit Threshold vs $\mathrm{R}_{\mathrm{ILIM}}$

## 10 Application and Implementation

## NOTE

Information in the following applications sections is not part of the Tl component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 10.1 Application Information

### 10.1.1 Constant-Current vs Latch-Off Operation and Impact on Output Voltage

Both the constant-current devices (TPS255x) and latch-off devices (TPS255x-1) operate identically during normal operation, that is, the load current is less than the current-limit threshold and the devices are not limiting current. During normal operation the $N$-channel MOSFET is fully enhanced, and $\mathrm{V}_{\text {OUT }}=\mathrm{V}_{\text {IN }}-\left(l_{\text {OUT }} \times r_{\text {DS(on) }}\right)$. The voltage drop across the MOSFET is relatively small compared to $\mathrm{V}_{\mathbb{I}}$, and $\mathrm{V}_{\text {OUT }} \neq \mathrm{V}_{\mathrm{IN}}$.
Both the constant-current devices (TPS255x ) and latch-off devices (TPS255x-1) operate identically during the initial onset of an overcurrent event. Both devices limit current to the programmed current-limit threshold set to $\mathrm{R}_{\text {IIIM }}$ by operating the N-channel MOSFET in the linear mode. During current-limit operation, the N-channel MOSFET is no longer fully-enhanced and the resistance of the device increases. This allows the device to effectively regulate the current to the current-limit threshold. The effect of increasing the resistance of the MOSFET is that the voltage drop across the device is no longer negligible ( $\mathrm{V}_{\mathbb{I N}} \neq \mathrm{V}_{\mathrm{OUT}}$ ), and $\mathrm{V}_{\text {OUT }}$ decreases. The amount that $\mathrm{V}_{\text {OUT }}$ decreases is proportional to the magnitude of the overload condition. The expected $\mathrm{V}_{\text {OUT }}$ can be calculated by,

$$
\mathrm{l}_{\mathrm{OS}} \times \mathrm{R}_{\text {LOAD }}
$$

where
$l_{O S}$ is the current-limit threshold and $R_{\text {LOAD }}$ is the magnitude of the overload condition.
For example, if $\mathrm{I}_{\text {OS }}$ is programmed to 1 A and a $1 \Omega$ overload condition is applied, the resulting $\mathrm{V}_{\text {OUT }}$ is 1 V .
While both the constant-current devices (TPS255x ) and latch-off devices (TPS255x-1) operate identically during the initial onset of an overcurrent event, they behave differently if the overcurrent event lasts longer than the internal delay de-glitch circuit ( $7.5-\mathrm{ms}$ typical). The constant-current devices (TPS255x ) assert the FAULT flag after the deglitch period and continue to regulate the current to the current-limit threshold indefinitely. In practical circuits, the power dissipation in the package increases the die temperature above the overtemperature shutdown threshold $\left(135^{\circ} \mathrm{C}\right.$ minimum), and the device turns off until the die temperature decreases by the hysteresis of the thermal shutdown circuit ( $10^{\circ} \mathrm{C}$ typical). The device turns on and continues to thermal cycle until the overload condition is removed. The constant-current devices resume normal operation once the overload condition is removed. The latch-off devices (TPS255x-1) assert the FAULT flag after the deglitch period and immediately turn off the device. The device remains off regardless of whether the overload condition is removed from the output. The latch-off devices remain off and do not resume normal operation until the surrounding system either toggles the enable or cycles power to the device.

### 10.2 Typical Applications

### 10.2.1 Two-Level Current-Limit Circuit

Some applications require different current-limit thresholds depending on external system conditions. Figure 24 shows an implementation for an externally controlled, two-level current-limit circuit. The current-limit threshold is set by the total resistance from ILIM to GND (see the Programming the Current-Limit Threshold section). A logiclevel input enables or disables MOSFET Q1 and changes the current-limit threshold by modifying the total resistance from ILIM to GND. Additional MOSFET and resistor combinations can be used in parallel to Q1/R2 to increase the number of additional current-limit levels.

## NOTE

ILIM must never be driven directly with an external signal.

## Typical Applications (continued)



Figure 24. Two-Level Current-Limit Circuit

### 10.2.1.1 Design Requirements

For this example, use the parameters shown in Table 1.
Table 1. Design Requirements

| PARAMETER | VALUE |
| :---: | :---: |
| Input voltage | 5 V |
| Output voltage | 5 V |
| Above a minimum current limit | 1000 mA |
| Below a maximum current limit | 500 mA |

### 10.2.1.2 Detailed Design Procedures

### 10.2.1.2.1 Designing Above a Minimum Current Limit

Some applications require that current limiting cannot occur below a certain threshold. For this example, assume that 1 A must be delivered to the load so that the minimum desired current-limit threshold is 1000 mA . Use the $\mathrm{l}_{\text {os }}$ equations and Figure 23 to select $\mathrm{R}_{\text {IIIM }}$.

$$
\begin{aligned}
& \mathrm{l}_{\mathrm{os} \text { min }}(\mathrm{mA})=1000 \mathrm{~mA}
\end{aligned}
$$

$$
\begin{align*}
& \mathrm{R}_{\text {ILIM }}(\mathrm{K} \Omega)=\left(\frac{25230 \mathrm{~V}}{\mathrm{losmin}^{\mathrm{OSA}}}\right)^{\frac{1}{1.016}} \\
& R_{\text {LLIM }}(k \Omega)=24 \mathrm{k} \Omega \tag{3}
\end{align*}
$$

Select the closest $1 \%$ resistor less than the calculated value: $R_{\text {ILIM }}=23.7 \mathrm{k} \Omega$. This sets the minimum current-limit threshold at 1 A . Use the Ios equations, Figure 23, and the previously calculated value for $\mathrm{R}_{\text {IIIM }}$ to calculate the maximum resulting current-limit threshold.

$$
\begin{align*}
& \mathrm{R}_{\text {ILIM }}(\mathrm{k} \Omega)=23.7 \mathrm{k} \Omega \\
& \mathrm{I}_{\text {OSmax }}(\mathrm{mA})=\frac{22980 \mathrm{~V}}{\mathrm{R}_{\text {ILIM }}^{0.94} \mathrm{k} \Omega} \\
& \mathrm{I}_{\text {OSmax }}(\mathrm{mA})=\frac{22980 \mathrm{~V}}{23.7^{0.94} \mathrm{k} \Omega} \\
& \mathrm{I}_{\text {OSmax }}(\mathrm{mA})=1172.4 \mathrm{~mA} \tag{4}
\end{align*}
$$

The resulting maximum current-limit threshold is 1172.4 mA with a $23.7-\mathrm{k} \Omega$ resistor.

### 10.2.1.2.2 Designing Below a Maximum Current Limit

Some applications require that current limiting must occur below a certain threshold. For this example, assume that the desired upper current-limit threshold must be below 500 mA to protect an up-stream power supply. Use the $\mathrm{I}_{\mathrm{OS}}$ equations and Figure 23 to select $\mathrm{R}_{\text {ILIM }}$.

$$
\begin{align*}
& \mathrm{I}_{\text {OSmax }}(\mathrm{mA})=500 \mathrm{~mA} \\
& \mathrm{I}_{\text {OSmax }}(\mathrm{mA})=\frac{22980 \mathrm{~V}}{\mathrm{R}_{\text {LIM }}{ }^{.9 \mathrm{k} \mathrm{k} \Omega}} \\
& \mathrm{R}_{\text {ILIM }}(\mathrm{k} \Omega)=\left(\frac{22980 \mathrm{~V}}{\mathrm{I}_{\text {OSmax }} \mathrm{mA}}\right)^{\frac{1}{0.94}} \\
& \mathrm{R}_{\text {ILIM }}(\mathrm{k} \Omega)=58.7 \mathrm{k} \Omega \tag{5}
\end{align*}
$$

Select the closest $1 \%$ resistor greater than the calculated value: $R_{\text {ILIM }}=59-k \Omega$. This sets the maximum currentlimit threshold at 500 mA . Use the $\mathrm{I}_{\text {OS }}$ equations, Figure 23 , and the previously calculated value for $\mathrm{R}_{\text {IIIM }}$ to calculate the minimum resulting current-limit threshold.

$$
\begin{align*}
& \mathrm{R}_{\mathrm{LLIM}}(\mathrm{k} \Omega)=59 \mathrm{k} \Omega \\
& \mathrm{I}_{\mathrm{OS} \text { min }}(\mathrm{mA})=\frac{25230 \mathrm{~V}}{\mathrm{R}_{\mathrm{LLIM}}^{1.016} \mathrm{k} \Omega} \\
& \mathrm{I}_{\mathrm{OS} \text { min }}(\mathrm{mA})=\frac{25230 \mathrm{~V}}{59^{1.016} \mathrm{k} \Omega} \\
& \mathrm{I}_{\mathrm{OS} \text { min }}(\mathrm{mA})=400.6 \mathrm{~mA} \tag{6}
\end{align*}
$$

The resulting minimum current-limit threshold is 400.6 mA with a $59-\mathrm{k} \Omega$ resistor.

### 10.2.1.2.3 Accounting for Resistor Tolerance

The previous sections described the selection of $R_{I L I M}$ given certain application requirements and the importance of understanding the current-limit threshold tolerance. The analysis focused only on the TPS255x and TPS255x1 performance and assumed an exact resistor value. However, resistors sold in quantity are not exact and are bounded by an upper and lower tolerance centered around a nominal resistance. The additional $\mathrm{R}_{\text {ILIM }}$ resistance tolerance directly affects the current-limit threshold accuracy at a system level. The following table shows a process that accounts for worst-case resistor tolerance assuming $1 \%$ resistor values. Step one follows the selection process outlined in the application examples above. Step two determines the upper and lower resistance bounds of the selected resistor. Step three uses the upper and lower resistor bounds in the los equations to calculate the threshold limits. It is important to use tighter tolerance resistors, for example, $0.5 \%$ or $0.1 \%$, when precision current limiting is desired.

Texas InSTRUMENTS

Table 2. Common RIIIM Resistor Selections

| DESIRED <br> NOMINAL CURRENT LIMIT (mA) | $\begin{aligned} & \text { IDEAL } \\ & \text { RESISTOR } \\ & (\mathbf{k} \Omega) \end{aligned}$ | CLOSEST 1\% RESISTOR (k $\Omega$ ) | RESISTOR TOLERANCE |  | ACTUAL LIMITS |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1\% LOW (k ${ }^{\text {a }}$ | $\begin{aligned} & \text { 1\% HIGHT } \\ & (\mathbf{k} \Omega) \end{aligned}$ | IOS MIN (mA) | IOS NOM (mA) | IOS MAX (mA) |
| 75 | SHORT ILIM to IN |  |  |  | 50.0 | 75.0 | 100.0 |
| 120 | 226.1 | 226 | 223.7 | 228.3 | 101.3 | 120.0 | 142.1 |
| 200 | 134.0 | 133 | 131.7 | 134.3 | 173.7 | 201.5 | 233.9 |
| 300 | 88.5 | 88.7 | 87.8 | 89.6 | 262.1 | 299.4 | 342.3 |
| 400 | 65.9 | 66.5 | 65.8 | 67.2 | 351.2 | 396.7 | 448.7 |
| 500 | 52.5 | 52.3 | 51.8 | 52.8 | 448.3 | 501.6 | 562.4 |
| 600 | 43.5 | 43.2 | 42.8 | 43.6 | 544.3 | 604.6 | 673.1 |
| 700 | 37.2 | 37.4 | 37.0 | 37.8 | 630.2 | 696.0 | 770.8 |
| 800 | 32.4 | 32.4 | 32.1 | 32.7 | 729.1 | 800.8 | 882.1 |
| 900 | 28.7 | 28.7 | 28.4 | 29.0 | 824.7 | 901.5 | 988.7 |
| 1000 | 25.8 | 26.1 | 25.8 | 26.4 | 908.3 | 989.1 | 1081.0 |
| 1100 | 23.4 | 23.2 | 23.0 | 23.4 | 1023.7 | 1109.7 | 1207.5 |
| 1200 | 21.4 | 21.5 | 21.3 | 21.7 | 1106.0 | 1195.4 | 1297.1 |
| 1300 | 19.7 | 19.6 | 19.4 | 19.8 | 1215.1 | 1308.5 | 1414.9 |
| 1400 | 18.3 | 18.2 | 18.0 | 18.4 | 1310.1 | 1406.7 | 1517.0 |
| 1500 | 17.0 | 16.9 | 16.7 | 17.1 | 1412.5 | 1512.4 | 1626.4 |
| 1600 | 16.0 | 15.8 | 15.6 | 16.0 | 1512.5 | 1615.2 | 1732.7 |
| 1700 | 15.0 | 15.0 | 14.9 | 15.2 | 1594.5 | 1699.3 | 1819.4 |

### 10.2.1.2.4 Input and Output Capacitance

Input and output capacitance improves the performance of the device; the actual capacitance must be optimized for the particular application. For all applications, TI recommends placing a $0.1-\mu \mathrm{F}$ or greater ceramic bypass capacitor between IN and GND as close to the device as possible for local noise de-coupling. This precaution reduces ringing on the input due to power-supply transients. Additional input capacitance may be needed on the input to reduce voltage overshoot from exceeding the absolute maximum voltage of the device during heavy transient conditions. This is especially important during bench testing when long, inductive cables are used to connect the evaluation board to the bench power-supply.

TI recommends placing a high-value electrolytic capacitor on the output pin when large transient currents are expected on the output.

### 10.2.1.3 Application Curves



Figure 25. Turnon Delay and Rise Time


Figure 26. Reverse-Voltage Protection Recovery

### 10.2.2 Auto-Retry Functionality

Some applications require that an overcurrent condition disables the part momentarily during a fault condition and re-enables after a pre-set time. This auto-retry functionality can be implemented with an external resistor and capacitor. During a fault condition, FAULT pulls low disabling the part. The part is disabled when EN is pulled low, and FAULT goes high impedance allowing $\mathrm{C}_{\text {RETRY }}$ to begin charging. The part re-enables when the voltage on EN reaches the turnon threshold, and the auto-retry time is determined by the resistor-capacitor time constant. The device continues to cycle in this manner until the fault condition is removed.


Figure 27. Auto-Retry Functionality
Some applications require auto-retry functionality and the ability to enable or disable with an external logic signal. Figure 28 shows how an external logic signal can drive EN through $\mathrm{R}_{\text {FAULT }}$ and maintain auto-retry functionality. The resistor-capacitor time constant determines the auto-retry time-out period.


Figure 28. Auto-Retry Functionality With External EN Signal

### 10.2.2.1 Design Requirements

For this example, use the parameters shown in Table 3.
Table 3. Design Requirements

| PARAMETER | VALUE |
| :---: | :---: |
| Input voltage | 5 V |
| Output voltage | 5 V |
| Current | 1200 mA |

### 10.2.2.2 Detailed Design Procedure

Refer to Programming the Current-Limit Threshold section for the current limit setting. For auto-retry functionality, once FAULT asserted, EN pull low, TPS2553 is disabled, FAULT des-asserted, $\mathrm{C}_{\text {RETRy }}$ is slowly charged to EN logic high through $\mathrm{R}_{\text {FAULT }}$, then enable, after deglitch time, FAULT asserted again. In the event of an overload, TPS2553 cycles and has output average current. ON-time with output current is decided by FAULT deglitch time. OFF-time without output current is decided by $\mathrm{R}_{\text {FAULT }} \times \mathrm{C}_{\text {RETRY }}$ constant time to EN logic high and $\mathrm{t}_{\mathrm{on}}$ time. Therefore, set the $\mathrm{R}_{\text {FAULT }} \times \mathrm{C}_{\text {RETRY }}$ to get the desired output average current during overload.

### 10.2.3 Typical Application as USB Power Switch



Figure 29. Typical Application as USB Power Switch

### 10.2.3.1 Design Requirements

For this example, use the parameters shown in Table 4.
Table 4. Design Requirements

| PARAMETER | VALUE |
| :---: | :---: |
| Input voltage | 5 V |
| Output voltage | 5 V |
| Current | 1200 mA |

### 10.2.3.1.1 USB Power-Distribution Requirements

USB can be implemented in several ways regardless of the type of USB device being developed. Several powerdistribution features must be implemented.

- SPHs must:
- Current limit downstream ports
- Report overcurrent conditions
- BPHs must:
- Enable or disable power to downstream ports
- Power up at < 100 mA
- Limit inrush current ( $<44 \Omega$ and $10 \mu \mathrm{~F}$ )
- Functions must:
- Limit inrush currents
- Power up at <100 mA

The feature set of the TPS255x and TPS255x-1 meets each of these requirements. The integrated current limiting and overcurrent reporting is required by self-powered hubs. The logic-level enable and controlled rise times meet the need of both input and output ports on bus-powered hubs and the input ports for bus-powered functions.

### 10.2.3.2 Detailed Design Procedure

### 10.2.3.2.1 Universal Serial Bus (USB) Power-Distribution Requirements

One application for this device is for current limiting in universal serial bus (USB) applications. The original USB interface was a $12-\mathrm{Mbps}$ or $1.5-\mathrm{Mbps}$, multiplexed serial bus designed for low-to-medium bandwidth PC peripherals (for example, keyboards, printers, scanners, and mice). As the demand for more bandwidth increased, the USB 2.0 standard was introduced increasing the maximum data rate to $480-\mathrm{Mbps}$. The four-wire USB interface is conceived for dynamic attach-detach (hot plug-unplug) of peripherals. Two lines are provided for differential data, and two lines are provided for $5-\mathrm{V}$ power distribution.
USB data is a $3.3-\mathrm{V}$ level signal, but power is distributed at 5 V to allow for voltage drops in cases where power is distributed through more than one hub across long cables. Each function must provide its own regulated 3.3 V from the $5-\mathrm{V}$ input or its own internal power supply. The USB specification classifies two different classes of devices depending on its maximum current draw. A device classified as low-power can draw up to 100 mA as defined by the standard. A device classified as high-power can draw up to 500 mA . It is important that the minimum current-limit threshold of the current-limiting power-switch exceed the maximum current-limit draw of the intended application. The latest USB standard must always be referenced when considering the current-limit threshold
The USB specification defines two types of devices as hubs and functions. A USB hub is a device that contains multiple ports for different USB devices to connect and can be self-powered (SPH) or bus-powered (BPH). A function is a USB device that is able to transmit or receive data or control information over the bus. A USB function can be embedded in a USB hub. A USB function can be one of three types included in the list below.

- Low-power, bus-powered function
- High-power, bus-powered function
- Self-powered function

SPHs and BPHs distribute data and power to downstream functions. The TPS255x has higher current capability than required for a single USB port allowing it to power multiple downstream ports.

## 11 Power Supply Recommendations

### 11.1 Self-Powered and Bus-Powered Hubs

A SPH has a local power supply that powers embedded functions and downstream ports. This power supply must provide between 4.75 V to 5.25 V to downstream facing devices under full-load and no-load conditions. SPHs are required to have current-limit protection and must report overcurrent conditions to the USB controller. Typical SPHs are desktop PCs, monitors, printers, and stand-alone hubs.
A BPH obtains all power from an upstream port and often contains an embedded function. It must power up with less than 100 mA . The BPH usually has one embedded function, and power is always available to the controller of the hub. If the embedded function and hub require more than 100 mA on power up, keep the power to the embedded function off until enumeration is completed. This can be accomplished by removing power or by shutting off the clock to the embedded function. Power-switching the embedded function is not necessary if the aggregate power draw for the function and controller is less than 100 mA . The total current drawn by the buspowered device is the sum of the current to the controller, the embedded function, and the downstream ports, and it is limited to 500 mA from an upstream port.

### 11.2 Low-Power Bus-Powered and High-Power Bus-Powered Functions

Both low-power and high-power bus-powered functions obtain all power from upstream ports. Low-power functions always draw less than 100 mA ; high-power functions must draw less than 100 mA at power up and can draw up to 500 mA after enumeration. If the load of the function is more than the parallel combination of $44 \Omega$ and $10 \mu \mathrm{~F}$ at power up, the device must implement inrush current limiting.

### 11.3 Power Dissipation and Junction Temperature

The low ON-resistance of the N-channel MOSFET allows small surface-mount packages to pass large currents. It is good design practice to estimate power dissipation and junction temperature. The below analysis gives an approximation for calculating junction temperature based on the power dissipation in the package. However, it is important to note that thermal analysis is strongly dependent on additional system level factors. Such factors include air flow, board layout, copper thickness and surface area, and proximity to other devices dissipating power. Good thermal design practice must include all system level factors in addition to individual component analysis.
Begin by determining the $r_{\text {DS(on) }}$ of the N-channel MOSFET relative to the input voltage and operating temperature. As an initial estimate, use the highest operating ambient temperature of interest and read $r_{D S(o n)}$ from the typical characteristics graph. Using this value, the power dissipation can be calculated using Equation 7.
$P_{D}=r_{D S(0 n)} \times I_{\text {OUT }}{ }^{2}$
where

- $P_{D}=$ Total power dissipation (W)
- $\mathrm{r}_{\mathrm{DS}(0 \mathrm{n})}=$ Power switch on-resistance ( $\Omega$ )
- $\mathrm{I}_{\text {Out }}=$ Maximum current-limit threshold $(\mathrm{A})$
- This step calculates the total power dissipation of the N -channel MOSFET.

Finally, calculate the junction temperature:

$$
T_{J}=P_{D} \times \theta_{J A}+T_{A}
$$

where

- $\mathrm{T}_{\mathrm{A}}=$ Ambient temperature ( ${ }^{\circ} \mathrm{C}$ )
- $\theta_{\mathrm{JA}}=$ Thermal resistance $\left({ }^{\circ} \mathrm{C} / \mathrm{W}\right)$
- $P_{D}=$ Total power dissipation (W)

Compare the calculated junction temperature with the initial estimate. If they are not within a few degrees, repeat the calculation using the refined $r_{\text {DS(on) }}$ from the previous calculation as the new estimate. Two or three iterations are generally sufficient to achieve the desired result. The final junction temperature is highly dependent on thermal resistance $\theta_{\mathrm{JA}}$, and thermal resistance is highly dependent on the individual package and board layout. The Thermal Information table provides example thermal resistances for specific packages and board layouts.

## 12 Layout

### 12.1 Layout Guidelines

- TI recommends placing the $100-\mathrm{nF}$ bypass capacitor near the IN and GND pins, and make the connections using a low-inductance trace.
- TI recommends placing a high-value electrolytic capacitor and a $100-\mathrm{nF}$ bypass capacitor on the output pin when large transient currents are expected on the output.
- The traces routing the RILIM resistor to the device must be as short as possible to reduce parasitic effects on the current limit accuracy.
- The PowerPAD must be directly connected to PCB ground plane using wide and short copper trace.


### 12.2 Layout Example



Figure 30. Layout Recommendation

## 13 Device and Documentation Support

### 13.1 Device Support

For the TI Switch Portfolio, go here.

### 13.2 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

Table 5. Related Links

| PARTS | PRODUCT FOLDER | SAMPLE \& BUY | TECHNICAL <br> DOCUMENTS |  <br> SOFTWARE |  <br> COMMUNITY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TPS32552 | Click here | Click here | Click here | Click here | Click here |
| TPS2553 | Click here | Click here | Click here | Click here | Click here |
| TPS2552-1 | Click here | Click here | Click here | Click here | Click here |
| TPS2553-1 | Click here | Click here | Click here | Click here | Click here |

### 13.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on Alert me to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 13.4 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

TI E2E ${ }^{\text {TM }}$ Online Community TI's Engineer-to-Engineer (E2E) Community. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.
Design Support TI's Design Support Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 13.5 Trademarks

PowerPAD, E2E are trademarks of Texas Instruments.
All other trademarks are the property of their respective owners.

### 13.6 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 13.7 Glossary

SLYZ022 - TI Glossary.
This glossary lists and explains terms, acronyms, and definitions.

## 14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

TEXAS
PACKAGE OPTION ADDENDUM
INSTRUMENTS
www.ti.com
19-Oct-2022

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material <br> (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS2552DBVR | ACTIVE | SOT-23 | DBV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | 2552 | Samples |
| TPS2552DBVR-1 | ACTIVE | SOT-23 | DBV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHX | Samples |
| TPS2552DBVT | ACTIVE | SOT-23 | DBV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | 2552 | Samples |
| TPS2552DBVT-1 | ACTIVE | SOT-23 | DBV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHX | Samples |
| TPS2552DRVR | ACTIVE | WSON | DRV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHR | Samples |
| TPS2552DRVR-1 | ACTIVE | WSON | DRV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHY | Samples |
| TPS2552DRVT | ACTIVE | WSON | DRV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 85 | CHR | Samples |
| TPS2552DRVT-1 | ACTIVE | WSON | DRV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHY | Samples |
| TPS2553DBVR | ACTIVE | SOT-23 | DBV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | 2553 | Samples |
| TPS2553DBVR-1 | ACTIVE | SOT-23 | DBV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHZ | Samples |
| TPS2553DBVT | ACTIVE | SOT-23 | DBV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | 2553 | Samples |
| TPS2553DBVT-1 | ACTIVE | SOT-23 | DBV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHZ | Samples |
| TPS2553DRVR | ACTIVE | WSON | DRV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHT | Samples |
| TPS2553DRVR-1 | ACTIVE | WSON | DRV | 6 | 3000 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CJZ | Samples |
| TPS2553DRVT | ACTIVE | WSON | DRV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CHT | Samples |
| TPS2553DRVT-1 | ACTIVE | WSON | DRV | 6 | 250 | RoHS \& Green | NIPDAU | Level-1-260C-UNLIM | -40 to 125 | CJZ | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design
PREVIEW: Device has been announced but is not in production. Samples may or may not be available
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free"
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption
Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a " $\sim$ " will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width

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OTHER QUALIFIED VERSIONS OF TPS2553, TPS2553-1 :

- Automotive : TPS2553-Q1, TPS2553-Q1

NOTE: Qualified Version Definitions:

- Automotive- Q100 devices qualified for high-reliability automotive applications targeting zero defects

PACKAGE MATERIALS INFORMATION
INSTRUMENTS

## TAPE AND REEL INFORMATION



QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE


| *All dimensions are nominal |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | Package <br> Type | Package <br> Drawing | Pins | SPQ | Reel <br> Diameter <br> $(\mathbf{m m})$ | Reel <br> Width <br> W1 (mm) | A0 <br> $(\mathbf{m m})$ | B0 <br> $(\mathbf{m m})$ | K0 <br> $(\mathbf{m m})$ | P1 <br> $(\mathbf{m m})$ | W <br> $(\mathbf{m m})$ | Pin1 <br> Quadrant |
| TPS2552DBVR | SOT-23 | DBV | 6 | 3000 | 180.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2552DBVR-1 | SOT-23 | DBV | 6 | 3000 | 178.0 | 9.0 | 3.23 | 3.17 | 1.37 | 4.0 | 8.0 | Q3 |
| TPS2552DBVR-1 | SOT-23 | DBV | 6 | 3000 | 179.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2552DBVT | SOT-23 | DBV | 6 | 250 | 180.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2552DBVT-1 | SOT-23 | DBV | 6 | 250 | 178.0 | 9.0 | 3.23 | 3.17 | 1.37 | 4.0 | 8.0 | Q3 |
| TPS2552DBVT-1 | SOT-23 | DBV | 6 | 250 | 179.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2552DRVR | WSON | DRV | 6 | 3000 | 180.0 | 8.4 | 2.3 | 2.3 | 1.15 | 4.0 | 8.0 | Q2 |
| TPS2552DRVR-1 | WSON | DRV | 6 | 3000 | 179.0 | 8.4 | 2.2 | 2.2 | 1.2 | 4.0 | 8.0 | Q2 |
| TPS2552DRVT | WSON | DRV | 6 | 250 | 180.0 | 8.4 | 2.3 | 2.3 | 1.15 | 4.0 | 8.0 | Q2 |
| TPS2552DRVT-1 | WSON | DRV | 6 | 250 | 179.0 | 8.4 | 2.2 | 2.2 | 1.2 | 4.0 | 8.0 | Q2 |
| TPS2553DBVR | SOT-23 | DBV | 6 | 3000 | 180.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2553DBVR-1 | SOT-23 | DBV | 6 | 3000 | 180.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2553DBVR-1 | SOT-23 | DBV | 6 | 3000 | 179.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2553DBVT | SOT-23 | DBV | 6 | 250 | 179.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2553DBVT | SOT-23 | DBV | 6 | 250 | 180.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2553DBVT-1 | SOT-23 | DBV | 6 | 250 | 179.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |


| Device | Package <br> Type | Package <br> Drawing | Pins | SPQ | Reel <br> Diameter <br> $(\mathbf{m m})$ | Reel <br> Width <br> W1 $(\mathbf{m m})$ | A0 <br> $(\mathbf{m m})$ | B0 <br> $(\mathbf{m m})$ | K0 <br> $(\mathbf{m m})$ | P1 <br> $(\mathbf{m m})$ | $\mathbf{W}$ <br> $(\mathbf{m m})$ | Pin1 <br> Quadrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS2553DBVT-1 | SOT-23 | DBV | 6 | 250 | 180.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |
| TPS2553DRVR | WSON | DRV | 6 | 3000 | 180.0 | 8.4 | 2.3 | 2.3 | 1.15 | 4.0 | 8.0 | Q2 |
| TPS2553DRVR-1 | WSON | DRV | 6 | 3000 | 180.0 | 8.4 | 2.3 | 2.3 | 1.15 | 4.0 | 8.0 | Q2 |
| TPS2553DRVT | WSON | DRV | 6 | 250 | 180.0 | 8.4 | 2.3 | 2.3 | 1.15 | 4.0 | 8.0 | Q2 |
| TPS2553DRVT-1 | WSON | DRV | 6 | 250 | 180.0 | 8.4 | 2.3 | 2.3 | 1.15 | 4.0 | 8.0 | Q2 |


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS2552DBVR | SOT-23 | DBV | 6 | 3000 | 210.0 | 185.0 | 35.0 |
| TPS2552DBVR-1 | SOT-23 | DBV | 6 | 3000 | 180.0 | 180.0 | 18.0 |
| TPS2552DBVR-1 | SOT-23 | DBV | 6 | 3000 | 203.0 | 203.0 | 35.0 |
| TPS2552DBVT | SOT-23 | DBV | 6 | 250 | 210.0 | 185.0 | 35.0 |
| TPS2552DBVT-1 | SOT-23 | DBV | 6 | 250 | 180.0 | 180.0 | 18.0 |
| TPS2552DBVT-1 | SOT-23 | DBV | 6 | 250 | 203.0 | 203.0 | 35.0 |
| TPS2552DRVR | WSON | DRV | 6 | 3000 | 210.0 | 185.0 | 35.0 |
| TPS2552DRVR-1 | WSON | DRV | 6 | 3000 | 200.0 | 183.0 | 25.0 |
| TPS2552DRVT | WSON | DRV | 6 | 250 | 210.0 | 185.0 | 35.0 |
| TPS2552DRVT-1 | WSON | DRV | 6 | 250 | 200.0 | 183.0 | 25.0 |
| TPS2553DBVR | SOT-23 | DBV | 6 | 3000 | 210.0 | 185.0 | 35.0 |
| TPS2553DBVR-1 | SOT-23 | DBV | 6 | 3000 | 210.0 | 185.0 | 35.0 |
| TPS2553DBVR-1 | SOT-23 | DBV | 6 | 3000 | 200.0 | 183.0 | 25.0 |
| TPS2553DBVT | SOT-23 | DBV | 6 | 250 | 200.0 | 183.0 | 25.0 |
| TPS2553DBVT | SOT-23 | DBV | 6 | 250 | 210.0 | 185.0 | 35.0 |
| TPS2553DBVT-1 | SOT-23 | DBV | 6 | 250 | 200.0 | 183.0 | 25.0 |
| TPS2553DBVT-1 | SOT-23 | DBV | 6 | 250 | 210.0 | 185.0 | 35.0 |
| TPS2553DRVR | WSON | DRV | 6 | 3000 | 182.0 | 182.0 | 20.0 |


| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS2553DRVR-1 | WSON | DRV | 6 | 3000 | 210.0 | 185.0 | 35.0 |
| TPS2553DRVT | WSON | DRV | 6 | 250 | 182.0 | 182.0 | 20.0 |
| TPS2553DRVT-1 | WSON | DRV | 6 | 250 | 210.0 | 185.0 | 35.0 |



## NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.25 per side.
4. Leads $1,2,3$ may be wider than leads $4,5,6$ for package orientation.
5. Refernce JEDEC MO-178.


SOLDER MASK DETAILS

NOTES: (continued)
6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.


SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL
SCALE:15X

NOTES: (continued)
8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.


Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE
WSON - 0.8 mm max height


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.


LAND PATTERN EXAMPLE
SCALE:25X


SOLDER MASK DETAILS

NOTES: (continued)
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
5. Vias are optional depending on application, refer to device data sheet. If some or all are implemented, recommended via locations are shown.


SOLDER PASTE EXAMPLE BASED ON 0.125 mm THICK STENCIL

NOTES: (continued)
6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

PACKAGE OUTLINE
WSON - 0.8 mm max height


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.




SOLDER MASK DEFINED

SOLDER MASK DETAILS

NOTES: (continued)
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
5. Vias are optional depending on application, refer to device data sheet. If some or all are implemented, recommended via locations are shown.


SOLDER PASTE EXAMPLE BASED ON 0.125 mm THICK STENCIL

NOTES: (continued)
6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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[^0]:    (1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
    (2) Voltages are referenced to GND unless otherwise noted.

[^1]:    (1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

